

METHOD FOR RECOVERING PRODUCTS

FIELD OF THE INVENTION

The present invention relates to a method comprising a multistep
5 process for recovering rhamnose and optionally arabinose. More particularly
the present invention relates to the use of a weakly acid cation exchange resin
in a chromatographic column in a multistep process.

BACKGROUND OF THE INVENTION

10 US Patent No. 2 684 331 (to Bauman) discloses a method for
separating chromatographically from one another two or more substances
having widely different ionization constants in which at least one of the
substances undergoes considerable ionization in a dilute aqueous solution
thereof. However, the method has not been used for separating sugars. The
15 examples of US Patent No. 2 684 331 describe separation of salts from
organic solvents, e.g. sodium chloride from formaldehyde. The method
comprises an ion exchange resin having an ion identical with an ion of highly
ionized solute. The ion exchange resin is either a cation exchange resin
having an acidic form or an anion exchange resin having a basic form. The
20 cation exchange resin contains sulphonic acid groups. The anion exchange
resin contains quaternary ammonium groups.

US Patent No. 2 911 362 (to Wheaton) describes a method
comprising a chromatographic separation process employing ion exchange
resins for separating two or more water soluble organic compounds from one
25 another in an aqueous medium in the absence of an ion exchange reaction,
i.e. in the substantial absence of a chemical reaction involving an absorption
of ions from the aqueous medium by the resin or the introduction of ions into
the solution from the resin. According to said method the ion exchange resin
can be either a cation exchange resin or an anion exchange resin. The cation
30 exchange resin may contain either sulfonic acid groups or carboxylic acid
groups. The anion exchange resin contains quaternary ammonium groups.
However, the method has not been used for separating sugars.

Chromatographic separation has been used for recovering xylose from hydrolysates of natural materials such as birch wood, corn cobs and cotton seed hulls in a method described in U.S. Patent No. 4 075 406 (to Melaja, et al.). The resin employed in the chromatographic separation is a strongly acid cation ex-changer, i.e. sulfonated polystyrene cross-linked with divinyl benzene.. The use of a strongly acid cation exchanger for separating monosaccharides, e.g. xylose, from magnesium sulfite cooking liquor is also known from Finnish Patent Application No. 962 609. The chromatographic separation is carried out by using a simulated moving bed. However, the separation of certain monosaccharides by using strongly acid cation exchange resins has turned out to be difficult. For instance the separation of rhamnose from other carbohydrates with strongly acid cation exchange resins and strongly basic cation exchange resins has been possible by using solvents such as alcoholic solvents as eluants (see e.g. Samuelson O., Chromatography on ion exchange resins, J. Methods Carbohy. Chem. 6 (1972) 65 - 75). In the described system anhydro sugars, such as rhamnose, have a shorter retention time than most of the aldoses and ketoses. Water would be a preferred eluant, but the use of water has not, however, been described in this connection. The problem when using water is that the various monosaccharides, such as rhamnose, xylose and arabinose, have almost similar retention times, whereby the fractions will overlap.

The separation of carbohydrates, especially xylose by strongly acid cation exchangers has been practiced industrially but is complicated. The method presented in US Patent No. 5 998 607 (to Heikkila, et al.) has been used especially for separating xylose from magnesium spent liquor. The problem has been the insufficient separation of xylose and xylonic acid and there is no suggestion of the use of a weakly acid cation exchange resin possibly giving a benefit for solving the problem. In the disclosed method the separation requires two steps. In the first step the cation exchange resin is used preferably in alkaline earth form, more preferably in Mg^{2+} form and in the second step the cation exchange resin is preferably in alkali-metal form (e.g. sodium). However, the separation of monosaccharides has also been found to

be unsatisfactory since all the other sugars elute at almost similar retention time with xylose. The pH used in the process low. The resin in a divalent form seemed to separate the xylose more effectively than the resin in a monovalent form.

5 Anion exchange resins have been used for separating fructose from glucose. Y. Takasaki (Agr. Biol. Chem. 36 (1972) pages 2575 - 77) and B. Lindberg et al. (Carbohyd. Res. 5 (1967), pages 286 - 291) describe the use of an anion exchanger in bisulfite form for the separation of sugars. However, the use of anion exchange resins does not result in good xylose separation
10 because xylose is overlapped by other sugars.

US Patent No. 4 358 322 (to Neuzil, et al.) discloses a process for separating fructose from a feed mixture comprising fructose and glucose. The process comprises contacting the mixture with an adsorbent comprising aluminosilicate or zeolite. The adsorbent contains one or more selected
15 cations at exchangeable cation sites. The cations are selected from the group consisting of sodium, barium and strontium. The cationic pairs used in the cationic sites are selected from the group consisting of barium and potassium and barium and strontium.

U.S. Patent No. 5 084 104 (to Heikkila, et al.) discloses a method
20 for the separation of xylose from a pentose-rich solution, e.g. birch wood. A chromatographic column which comprises a strongly basic anion exchange resin is used. The anion exchange resin is in sulfate form. Using this method xylose is retarded most strongly and the other monosaccharides are eluted faster.

25 A method for preparing of L-arabinose is known from the publication WO 99/57326 where the process is characterized by contacting plant fibers with an acid to hydrolyze the fibers under such conditions that the L-arabinose ingredients contained in the plant fibers are selectively obtained. U.S. Patent No. 4 880 919 (to Kulprathipanja) discloses a process for separating arabinose
30 from mixtures of monosaccharides containing arabinose and other aldopentoses and aldohexoses by adsorption on sulfonated polystyrene divinyl benzene crosslinked ion exchange resins exchanged with Ca^{2+} and NH_4^+ ions

and desorbing the adsorbate with water. A process for producing crystalline L-arabinose is known from U.S. Patent No. 4 816 078 (to Schiweck, et al.).

The preparation of arabinose is also known from US Patent No. 4 664 718 (to Chang). In the described method, arabinose is separated
5 from a mono-saccharide mixture containing also other aldopentoses and aldohexoses. The feed is contacted with with a calcium-Y-type or calcium-X-type zeolite and arabinose is adsorbed selectively. The desorption is conducted with water or ethanol.

Publication DE 3 545 107 describes a method for the preparation of
10 rhamnose from arabic gum. A strongly acid cation exchange resin is used for the separation of sugars and rhamnose by adsorption with activated charcoal. Arabinose is also separated by this method.

Barker, S.A. et al (Carbohydrate Research, 26 (1973) 55 - 64) have described the use of poly(4-vinylbenzeneboronic acid) resins in the fractiona-
15 tion and interconversion of carbohydrates. In the method water is used as an eluant. The best yield of fructose was received when the pH was high. The resins have also been used to displace the pseudo equilibrium established in aqueous alkali between D-glucose, D-fructose and D-mannose to yield D-fructose.

20 CA Patent No. 1 249 812 discloses a multistep process for the separation of sugars and lignosulphonates from sulphite spent liquor. The process comprises the steps of (a) introducing sulphite spent liquor having a certain pH into a chromatographic column containing a resin in metal salt form, (b) eluting the column with water to obtain a substantially sugar-free
25 lignosulphonate-rich fraction and a sugar-rich fraction, (c) collecting the sugar-rich fraction for further purification, (d) adjusting the pH of the fraction to a certain level and introducing it to a second column containing a resin in monovalent metal salt form, and (e) eluting the sugar-rich material from the second column to obtain a sugar-rich fraction and a lignosulphonate-rich
30 fraction. The process of said CA patent does not include the use of a weakly acid cation exchange resin for chromatographic separation.

A process for crystallizing xylose is known from Finnish Patent 97 625. In the process xylose is recovered by crystallization from the solutions in which the xylose purity is relatively low. Especially the process concerns recovering xylose from biomass derived solutions.

5 When xylose is prepared by hydrolysing biomass derived xylose rich hemicellulose the mixture contains among xylose also glucose, galactose, rhamnose, mannose and arabinose. It also may contain acetic acid and uronic acids such as galacturonic acid and glucuronic acid. The hydrolysing acid and the uronic acid are generally easily removed by ion exclusion. However, it has
10 been difficult to fractionate monosaccharide mixtures to their components.

Surprisingly it has been found that rhamnose and, if desired, arabinose can be effectively separated from carbohydrate streams by using weakly acid cation exchange resins. The order of elution seems to be, besides other factors, affected strongly by the hydrophobic/hydrophilic interaction
15 between the carbohydrate and the resin. If the resin is in hydrophilic form, the most hydrophobic carbohydrate seems to elute first and the most hydrophilic last. For instance, the resin in H^+ form seems to be less hydrophilic than the resin in Na^+ form. The different elution order of components in a chromatographic column using a weakly acid cation exchange resin can be
20 effectively used in the method of the present invention comprising a multistep process.

SUMMARY OF THE INVENTION

The above mentioned objects and others are accomplished by the
25 present invention, which relates to a method for recovering a monosaccharide selected from the group consisting of rhamnose, arabinose, xylose and mixtures thereof from a solution containing at least two of said monosaccharides by a multistep process using chromatographic separation comprising at least one step, where a weakly acid cation exchange resin is
30 used for the chromatographic separation. The method may preferably contain additional steps comprising the use of chromatographic columns containing strongly acid cation exchange resins, evaporation, crystallization, etc.

BRIEF DESCRIPTION OF THE DRAWINGS

The following drawings are illustrative embodiments of the invention and are not meant to limit the scope of the invention as defined in the claims.

5 FIG. 1 is a graphical presentation of the elution profiles and pH according to Example 1.

 FIG. 2 is a graphical presentation of the elution profiles and pH according to Example 2.

10 FIG. 3 is a graphical presentation of the elution profiles and pH according to Example 3.

 FIG. 4 is a graphical presentation of the elution profiles and pH according to Example 4.

 FIG. 5 is a graphical presentation of the elution profiles and pH according to Example 5.

15 FIG. 6 is a graphical presentation of the elution profiles and pH according to Example 6.

 FIG. 7 is a graphical presentation of the elution profiles and pH according to Example 7.

20 FIG. 8 and 9 are schematic presentations of embodiments of the present invention.

DETAILED DESCRIPTION OF THE INVENTION

According to the present invention a solution containing a monosaccharide selected from the group consisting of rhamnose, arabinose, 25 xylose and mixtures thereof is subjected to a multistep process using chromatographic separation comprising at least one step, where a weakly acid cation exchange resin is used in a chromatographic column or part of it. The multi-step process according to the invention may preferably comprise additional steps, such as steps using chromatographic columns containing 30 strongly acid cation exchange resins, evaporation, crystallization, etc. in order to enhance the effective separation of the desired product. Suitable starting solutions are those obtained by hydrolyzing hemicellulose. In addition to

rhamnose the starting solution preferably contains arabinose and possibly
 xylose. Such solutions are for instance xylose process streams and side
 streams. In addition to rhamnose also other carbohydrates may be recovered
 by the method of the present invention. Such carbohydrates are e.g.
 5 monosaccharides, such as arabinose, preferably L-arabinose, xylose,
 preferably D-xylose and mixtures thereof. The general opinion has been that
 an effective separation of the monosaccharides in question requires the use,
 for instance, of ion exclusion and size exclusion. The additional feature
 relating to the use of a weakly acid cation exchange resin is that if the resin
 10 is in hydrophilic form the most hydrophobic monosaccharide seems to be
 eluted first and the most hydrophilic monosaccharide is eluted last. The
 solution containing rhamnose treated may be a product obtained from the
 processing of hydrolysates or prehydrolysates of hemicellulose from hard
 wood and xylose containing biomass, e.g. solutions formed in paper and
 15 dissolving pulp processing, for example siccating or prehydrolysis of sa-
 cccooking.

The chromatographic column used in the method of the present
 invention is filled with a weakly acid cation exchange resin, preferably an
 acrylic cation exchange resin having carboxylic functional groups. However,
 20 the resin can be other than an acrylic resin and the functional group can be
 other than a carboxylic group, e.g. another weak acid. Such an acrylic resin is
 preferably derived from methyl acrylate, ethyl acrylate, buthyl acrylate,
 methylmethacrylate or acrylonitrile or acrylic acids or mixtures thereof. The
 resin may be crosslinked with a cross-linking agent, e.g. divinyl benzene
 25 (DVB). A suitable crosslinking degree is 1 to 20 % by weight, preferably 3 to 8
 % by weight. The average particle size of the resin is normally 10 to 2000 μm ,
 preferably 100 to 400 μm . The resin may be regenerated into H^+ , Na^+ , Mg^{2+} or
 Ca^{2+} form. However, also other ionic forms may be used.

The column is preferably eluted at temperatures from 10 to 95 $^{\circ}\text{C}$,
 30 more preferably from 30 to 95 $^{\circ}\text{C}$, more preferably from 55 to 85 $^{\circ}\text{C}$. It is
 known that a higher separation temperature decreases the viscosity and
 improves the separation performance.

The eluant used in the chromatographic separation according to the present invention is either water, a solvent, e.g. an alcohol, or a mixture thereof. Preferably the eluant is water.

The carbohydrate solution to be fractioned is optionally filtrated
5 before chromatographic separation, whereby the filtration may be carried out by using a pressure filter and diatomaceous earth as a filter aid. The pH of the feed solution is optionally adjusted to 1 to 10, preferably 2 to 10, more preferably 2 to 4 and 5 to 10. For instance when pH is high, i.e. 6 to 7, rhamnose is separated first before other more hydrophilic monosaccharides.
10 After the pH has been adjusted the solution may be filtered. The dry substance of the feed solution is adjusted to an appropriate level before chromatographic separation.

A feeding device is used for feeding the solution to the column. The temperature of the column, feed solution and eluant is most preferably
15 approximately 65 °C. This is accomplished by preheating the feed solution. The feed solution is eluted in the column by feeding water, for instance demineralized water or e.g. condensate or some other aqueous solution, alcohol or a mixture thereof into the column. The eluant may be pumped through a heat ex-changer as well. The flow rate in the column is adjusted to
20 an appropriate level. The fractions of the outcoming solutions are collected at suitable intervals and analyzed. The outcome from the column may be monitored by on-line instruments. The fractionated products, e.g. rhamnose and arabinose, may be isolated by crystallization afterwards or in the following step. Also recycle fractions collected from the other end of the column may be
25 used in a way known per se.

It is clear for the person skilled in the art that the multistep process can be altered by reorganizing the order of the process units or by adding or removing some process units. The person skilled in the art may also add or alter the order of other separation, recovering and concentration units.

30 Further, it is possible to arrange two or more chromatographic columns in sequence wherein at least one column contains a weakly acid cation exchange resin, the other columns possibly containing a strongly acid

cation exchange resin. Also simulated moving bed (SMB) systems may be used. The simulated moving bed system can be either sequential or continuous. In a preferred embodiment of the invention a first column containing a strongly acid cation exchange resin is connected to a second column containing a weakly acid cation exchange resin. Fractions obtained from the second column may be lead to one or more further columns containing either strongly acid or weakly acid cation exchange resins. Such an arrangement further improves the separation performance and increases the yields and purity of the products such as rhamnose, arabinose and xylose. Between the columns there are optionally additional process steps comprising, e.g. precipitation, filtration, crystallization, evaporation or some other concentration process steps or other known process units.

In the multistep process according to the present invention where a weakly acid cation exchange resin is used the elution order of rhamnose and other saccharides is advantageously different from the elution order obtained by using strongly basic resins in bisulfite form or sulfate form or using strongly acid cation exchange resins. One of the advantages relating to the present invention is that different elution order of the components in the chromatographic column is advantageously used in the method of the invention comprising a multistep process. One of the product fractions received is a rhamnose rich fraction, one is a xylose rich fraction, and one is a arabinose rich fraction. According to the multistep process of the present invention using a weakly acid cation exchange resin in a first step rhamnose is preferably eluted before the other monosaccharides, when the resin is in hydrophilic form. This allows rhamnose, and also the other carbohydrates, to be received in good yields with high purity. When the resin is in a more hydrophobic form, rhamnose is eluted in the back slope of the monosaccharide separation.

Figure 8 presents a schematic drawing where crystalline xylose is produced. The crystallization mother liquor is used in a multistep process for producing rhamnose, comprising at least one step using a weakly acid cation exchange resin.

Figure 9 shows a more detailed example of a multistep process for producing rhamnose. At first xylose is purified in the xylose process and a xylose fraction is recovered. Also an arabinose fraction may be collected. The crystallization mother liquor of the xylose process is further purified by chromatographic separation. The resin may be a weakly acid or strongly acid cation exchange resin. The separation is continued by chromatographic separation and a rhamnose rich fraction is recovered. Again, a weakly acid or strongly acid cation exchange resin can be used. The rest of the outflow can be further separated using a strongly acid cation exchange resin and more xylose can be recovered. Also arabinose may be collected at this step.

Also the rhamnose rich fraction is further purified by using either a weakly or strongly acid cation exchange resin. However, at least one of the three chromatographic separation steps for the rhamnose fraction is carried out by using a weakly acid cation exchange resin.

Rhamnose crystallization may be carried out after the last separation step. The product obtained is suitably rhamnose monohydrate.

The method according to the present invention makes it possible to separate and recover rhamnose and also other products, such as rhamnose, arabinose and xylose, in good yields from solutions containing rhamnose, which has been very difficult by known methods using e.g. strongly acid cation exchange resins. One of the advantages achieved by the method of the present invention over the prior art is that the use of a weakly acid cation exchange resin allows the use of water as an eluant for efficient separation. Known methods using strongly acid cation exchange resins for efficient separation of carbohydrate products of the type mentioned above always require that the eluant is a solvent, e.g. aqueous alcohol. However, when water is used as the eluant, the handling is easier, the costs are lower and the safety is higher. By using water as the sole eluant, problems relating to storage and regeneration, for example, are avoided.

The following examples illustrate the present invention. The examples are not to be construed to limit the claims in any manner whatsoever.

Example 1

Chromatographic separation of xylose crystallization run-off with a H^+/Mg^{2+} -form resin

Xylose crystallization run-off which was beech wood based Mg-base
 5 si-cooking liquor was subjected to a chromatographic separation. The separation was performed in a laboratory chromatographic separation column as a batch process. The column with a diameter of 0.045 m was filled with an acrylic weakly acid cation exchange resin (Finex CA 12 GCTM) manufactured by Finex Oy, Finland. The resin was an ethyl acrylate -based resin. The height
 10 of the resin bed was about 0.70 m. The cross-linkage degree of the resin was 6 % by weight DVB and the average particle size of the resin was 0.26 mm. The resin was regenerated into mainly H^+ -form (94% by equivalent) and partly Mg^{2+} -form (6% by equivalent) and a feeding device was placed at the top of the resin bed. The temperature of the column and feed solution and eluant
 15 water was approximately 65°C. The flow rate in the column was adjusted to 4 ml/min.

The chromatographic separation was carried out as follows:

Step 1:

The dry substance of the feed solution was adjusted to 25 g dry
 20 substance in 100 g solution according to the refractive index (RI) of the solution. The pH of the feed solution was 3.5.

Step 2:

100 ml of preheated feed solution was pumped to the top of the resin bed.

Step 3:

25 The feed solution was eluted downwards in the column by feeding preheated ion-exchanged water to the top of the column.

Step 4:

10 ml samples of the outcoming solution were collected at 3 min intervals. The composition of the samples was analysed with Dionex HPLC
 30 equipment with pulsed electrochemical detector and CarboPac PA1TM anion exchange column (water and 0.2 M NaOH as eluants).

The resin gives a good separation of rhamnose and arabinose from other monosaccharides. Rhamnose and arabinose are eluted at the end of the profile. The pH of the effluent was between 3 and 4. The results are shown graphically in FIG. 1.

5

Example 2

Purification of L-rhamnose by chromatographic separation

Xylose precipitation crystallization (the final run-off) mother liquor from birch wood based si-cooking was used as a starting material and was thus subjected to a chromatographic separation in a batch separation column.

10

The separation was performed in a pilot chromatographic separation column as a batch process. The whole equipment consisted of a feed tank, a feed pump, a heat exchanger, a chromatographic separation column, product containers, pipelines for input of feed solution as well as eluant water, pipelines for output and flow controlling equipments.

15

The column with a diameter of 0.225 m was filled with an acrylic weakly acid cation exchange resin (manufactured by Finex Ltd., Finland); the height of the resin bed was about 5.2 m. The degree of cross-linkage was 3 % by weight DVB and the average particle size was 0.34 mm. The resin was re-generated into sodium (Na^+) form and a feeding device was then placed at the top of the resin bed. The temperature of the column, feed solution and eluant water was 65 °C. The flow rate in the column was adjusted to 40 l/h.

20

The feed solution was pre-treated first by filtration, which was done using a pressure filter and diatomaceous earth as filter aid. The feed solution was then heated to 65 °C and the pH was adjusted to pH 6.0 with sodium hydroxide solution, after which the solution was filtered.

25

Chromatographic separation was carried out as follows:

Step1:

The dry substance of the feed solution was adjusted to 35 g dry substance in 100 g of solution according to the refractive index (RI) of the solution.

30

Step2:

20 l of preheated feed solution was transferred to the top of the resin bed.

Step 3:

The feed solution was eluted downwards in the column by feeding
5 ion exchanged preheated water to the top of the column.

Step 4:

The density and conductivity of the outcoming solution were measured continuously and according to this information, the outcoming solution was collected and divided into two fractions (when the feed profiles were
10 overlapping) in the following order: rhamnose fraction (containing most of the rhamnose) and xylose fraction (containing most of the xylose, other saccharides and salts). The sequential feeds can also be done without overlapping and thus the outcoming solution can be divided into four fractions in the following order: residual fraction number one (containing salts), rhamnose
15 fraction (containing most of the rhamnose), xylose fraction (containing most of the xylose and some other monosaccharides) and residual fraction number two (containing other monosaccharides). Optionally between the outcoming fractions can be taken recycle fractions which can be recycled for diluting the feed or which can be fed as such into the column.

20 The amount of dry substance as well as rhamnose and xylose content in the feed solution and in product fractions are presented in Table 1. The concentrations of the successive components are expressed as percentages of the total dry substance in the particular fraction. The yield of rhamnose and xylose in product fractions are also presented (the amount of the component
25 in the particular fraction in relation to the total amount of that component in all outcoming fractions).

Table1. Compositions and yields (when profiles were overlapping and the outcoming solution was divided in two fractions)

	<u>Feed solution</u>	<u>Rhamnose fraction</u>	<u>Xylose fraction</u>
DS in fraction, kg	8.0	2.2	5.8
DS g/100 g solution	30.0	8.9	15.5
Rhamnose, % of DS in fraction	5.5	18.0	0.8
Xylose, % of DS in fraction	22.5	13.2	25.6
Rhamnose, yield %		90.0	10.0
Xylose, yield %		17.0	83.0

5

The pH of the effluent was between 7.3 and 9.3. The results are shown graphically in FIG. 2.

10

Example 3

Chromatographic separation of xylose-arabinose fraction from rhamnose separation

Arabinose containing xylose fraction, prepared as in Example 2, from rhamnose separation was subjected to a chromatographic separation.

15 The separation was performed in a pilot chromatographic separation column as a batch process. The column with a diameter of 0.225 m was filled with a strong acid cation exchange resin (Finex CS 13 GCTM, manufactured by Finex Oy, Finland). The height of the resin bed was 5.0 m. The cross-linkage degree of the resin was 5.5 % by weight DVB and the average particle size about

20 0.4 mm. The resin was in Ca²⁺ -form. A feeding device was placed at the top of the resin bed. The temperature of the column, feed solution and eluant water was approximately 65 °C. The flow rate in the column was adjusted to 30 l/h. A check filtration (through a filter bag) was made prior the separation.

The chromatographic separation was carried out as follows:

Step 1:

The dry substance of the feed solution was adjusted to 30 g dry substance in 100 g solution according to the refractive index (RI) of the solution:

5

Step 2:

15 litres of preheated feed solution was pumped to the top of the resin bed.

Step 3:

10 The feed solution was eluted downwards in the column by feeding preheated ion-exchanged water to the top of the column.

Step 4:

15 The density and conductivity of the outcoming solution were measured continuously. The outcoming solution was collected and divided into three fractions in the following order: residual fraction (containing some of the xylose), xylose rich fraction (containing most of the xylose and other monosaccharides) and arabinose rich fraction (containing most of the arabinose). The amount of dry substance as well as arabinose and xylose content in the feed solution and in product fractions are presented in table 2. The concentrations of the components are expressed as percentages of the total dry substance in the particular fraction. The yield of arabinose and xylose in product fractions is also presented (the amount of the component in the particular fraction in relation to the total amount of that component in all outcoming fractions).

25

30

Table 2. : Compositions and yields

	<u>Feed solution</u>	<u>Xylose fraction</u>	<u>Arabinose fraction</u>
5 DS in fraction, kg	5.0	3.3	1.7
DS g/100 g solution	30		
Arabinose, %	3.7	0.5	10.0
Xylose, %	36.5	44.0	21.0
10 Arabinose, yield %		10.0	90.0
Xylose, yield %		80.0	20.0

15 Arabinose was eluting at the back slope of the profile. Galactose and mannose and especially glucose and xylose can be separated from arabinose effectively. The arabinose content (% of the total dry substance) in the arabinose rich product fraction was 3-fold compared to the arabinose content in feed solution and the arabinose recovery was then 90 %.

20 The pH of the effluent is between 5.3 and 6. The results are shown graphically in FIG. 3.

Example 4

Chromatographic separation of xylose crystallization run-off with a Na⁺ -form strong acid cation exchange resin

25 Xylose precipitation crystallization run-off which was birch wood based Ca-base si-cooking liquor was subjected to a chromatographic separation in a batch separation column. The separation was performed in a pilot scale chromatographic separation column as a batch process.

30 The whole equipment consisted of a feed tank, a feed pump, a heat exchanger, a chromatographic separation column, product containers, pipelines for input of feed solution as well as eluant water, pipelines for output and flow control for the outcoming liquid.

The column with a diameter of 0.225 m was filled with a strongly acid cation exchange resin (manufactured by Finex Ltd, Finland). The height of the resin bed was approximately 5.1 m. The degree of cross-linkage was 5.5 % by weight DVB and the average particle size of the resin was 0.41 mm.

- 5 The resin was regenerated into sodium (Na^+) form and a feeding device was placed at the top of the resin bed. The temperature of the column, feed solution and eluant water was approximately 65 °C. The flow rate in the column was adjusted to 30 l/h.

- 10 The feed solution was pre-treated by filtration by using a pressure filter and diatomaceous earth as filter aid. The feed solution was then heated to 65 °C and the pH was adjusted to pH 6, after which the solution was filtered via filter.

Chromatographic separation was carried out as follows:

Step 1.

- 15 The dry substance of the feed solution was adjusted to 35 g dry substance in 100 g of solution according to the refractive index (RI) of the solution.

Step 2.

- 20 15 l of the preheated feed solution was pumped to the top of the resin bed.

Step 3.

The feed solution was eluted downwards in the column by feeding preheated ion-exchanged water to the top of the column.

25

Step 4.

- 30 The density and conductivity of the outcoming solution were measured continuously. The outcoming solution was collected and divided into two fractions in the following order:

residual fraction (containing most of the salts) and xylose fraction (containing xylose, rhamnose, arabinose and other monosaccharides).

The amount of dry substance as well as rhamnose, arabinose and xylose content in the feed solution and in product fraction (xylose fraction) are presented in table 3. The concentrations of the components are expressed as percentages of the total dry substance in the particular fraction. The yield of rhamnose, arabinose and xylose in product fraction are also presented (the amount of the component in the particular fraction in relation to the total amount of that component in all outcoming fractions). The colour (ICUMSA, measured at pH 5) of the feed solution and product fraction are also presented as well as colour removal %.

Table 3.: Compositions, yields and colors

	<u>Feed solution</u> <u>fraction</u> (nominal)	<u>Xylose fraction</u> (analyzed from samples)	<u>Residual</u> (analyzed from samples)
DS in fraction, kg	5.9	4.3	2.1
DS g/100 g solution	34.5	9.3	3.5
Rhamnose, %	5.6	7.1	0.04
Arabinose, %	2.8	3.9	0.03
Xylose, %	26.0	37.7	0.1
Color, ICUMSA	38 900	5 000	
Rhamnose, yield %		99.7	
Arabinose, yield %		99.6	
Xylose, yield %		99.9	
Colour removal, %		87.1	

Most of the salts and color were removed from xylose precipitation crystallization run-off with a Na^+ -form strong acid cation exchange resin. Also the amounts of rhamnose, arabinose and xylose were higher in the product fraction than in the feed solution. The pH of the effluent was between 5.5 and 7.2. The results are shown graphically in FIG. 4.

Example 5

Chromatographic separation of rhamnose containing xylose fraction

Xylose fraction prepared according to example 4 (containing xylose, rhamnose, arabinose and other monosaccharides) was subjected to a chromatographic separation in a batch separation column. The separation was performed in a pilot scale chromatographic separation column as a batch process.

The whole equipment consisted of a feed tank, a feed pump, a heat exchanger, a chromatographic separation column, product containers, pipelines for input of feed solution as well as eluant water, pipelines for output and flow control for the outcoming liquid.

The column with a diameter of 1.0 m was filled with a weakly acid cation exchange resin (Finex CA 16 GCTM) manufactured by Finex Ltd, Finland. The resin was methyl acrylate –based resin. The height of the resin bed was approximately 5.0 m. The degree of cross-linkage was 8 % by weight DVB and the average particle size of the resin was 0.28 mm. The resin was regenerated into sodium (Na⁺) form and a feeding device was placed at the top of the resin bed. The temperature of the column, feed solution and eluant water was 65°C. The flow rate in the column was adjusted to 785 l/h.

The pH of the feed solution was adjusted to pH 6.5 after which the solution was filtered via filter.

Chromatographic separation was carried out as follows:

Step 1.

The dry substance of the feed solution was adjusted to 35 g dry substance in 100 g of solution according to the refractive index (RI) of the solution.

Step 2.

400 l of the preheated feed solution was pumped to the top of the resin bed.

Step 3.

The feed solution was eluted downwards in the column by feeding preheated ion-exchanged water to the top of the column.

Step 4.

The density and conductivity of the outcoming solution were measured continuously. The outcoming solution was collected and divided into three fractions (when the feed profiles were not overlapping) in the following order: residual fraction (containing most of the salts), rhamnose rich fraction (containing most of the rhamnose) and xylose rich fraction (containing most of the xylose, arabinose and other monosaccharides).

10

The amount of dry substance as well as rhamnose and xylose content in the feed solution and in product fractions are presented in table 4. The concentrations of the components are expressed as percentages of the total dry substance in the particular fraction. The yield of rhamnose and xylose in product fractions is also presented (the amount of the component in the particular fraction in relation to the total amount of that component in all outcoming fractions).

15

Table 4. : Compositions and yields

		<u>Feed solution</u>	<u>Rhamnose fraction</u>	<u>Xylose fraction</u>
5	DS in fraction, kg	160	44	114
	DS g/100 g solution	36.1	6.2	10.6
	Rhamnose, %	6.7	21.9	0.9
	Xylose, %	37.4	24.5	36.5
10	Rhamnose, yield %		90.4	--
	Xylose, yield %		--	79.0

Rhamnose content (% of the total dry substance) in rhamnose rich product fraction was 3,3-fold compared to rhamnose content in feed solution. Rhamnose was separated from feed solution with a good yield. The pH of the effluent was between 8 and 9. The results are shown graphically in FIG. 5. Arabinose can be separated from the xylose fraction for example by using a strongly acid cation exchange resin.

20 **Example 6**

Chromatographic separation of rhamnose rich fraction with a weakly acid cation exchange resin

Rhamnose rich fraction prepared according to example 5 was subjected to a chromatographic separation in a batch separation column. The separation was performed in a pilot scale chromatographic separation column as a batch process.

The whole equipment consisted of a feed tank, a feed pump, a heat exchanger, a chromatographic separation column, product containers, pipelines for input of feed solution as well as eluant water, pipelines for output and flow control for the outcoming liquid.

The column with a diameter of 1.0 m was filled with a weakly acid cation exchange resin (Finex CA 16 GCTM) manufactured by Finex Ltd,

Finland. The resin was methyl acrylate –based resin. The height of the resin bed was approximately 5.0 m. The degree of cross-linkage was 8 w-% DVB and the average particle size of the resin was 0.28 mm. The resin was regenerated into sodium (Na^+) form and a feeding device was placed at the top of the resin bed. The temperature of the column, feed solution and eluant water was 65°C. The flow rate in the column was adjusted to 785 l/h.

The pH of the feed solution was adjusted to pH 6.5 after which the solution was filtered via filter.

10 Chromatographic separation was carried out as follows:

Step 1.

The dry substance of the feed solution was adjusted to 35 g dry substance in 100 g of solution according to the refractive index (RI) of the solution.

15 Step 2.

250 l of the preheated feed solution was pumped to the top of the resin bed.

Step 3.

The feed solution was eluted downwards in the column by feeding preheated ion-exchanged water to the top of the column.

Step 4.

The density and conductivity of the outcoming solution were measured continuously. The outcoming solution was collected and divided into three fractions (when the feed profiles were not overlapping) in the following order: first residual fraction (containing most of the salts), rhamnose rich fraction (containing most of the rhamnose) and second residual fraction (containing most of the xylose and other monosaccharides).

The amount of dry substance as well as rhamnose and xylose content in the feed solution and in product fraction are presented in table 5. The concentrations of the components are expressed as percentages of the total dry substance in the particular fraction. The yield of rhamnose in product

fraction is also presented (the amount of the component in the particular fraction in relation to the total amount of that component in all outcoming fractions).

5 Table 5. : Compositions and yields

	<u>Feed solution</u>	<u>Rhamnose fraction</u>
DS in fraction, kg	100	39
10 DS g/100 g solution	35.5	8.6
Rhamnose, %	21.6	47.0
Xylose, %	23.1	6.2
Rhamnose, yield %		86.0

15

The rhamnose content (% of the total dry substance) in product fraction was 2,2-fold compared to rhamnose content in feed solution. Rhamnose was separated from feed solution with a good yield. The pH of the effluent was between 8 and 10. The results are shown graphically in FIG. 6.

20

Example 7

Chromatographic separation of rhamnose rich fraction with a Ca^{2+} -form strong acid cation exchange resin

Rhamnose rich fraction prepared according to example 6 was subjected to a chromatographic separation in a batch separation column. The separation was performed in a pilot scale chromatographic separation column as a batch process.

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The whole equipment consisted of a feed tank, a feed pump, a heat exchanger, a chromatographic separation column, product containers, pipelines for input of feed solution as well as eluant water, pipelines for output and flow control for the outcoming liquid.

30

The column with a diameter of 0.6 m was filled with a strong acid cation exchange resin (Finex CS 11 GC) manufactured by Finex Ltd, Finland.

The height of the resin bed was approximately 5.0 m. The degree of cross-linkage was 5.5 w-% DVB and the average particle size of the resin was 0.40 mm. The resin was regenerated into sodium (Ca^{2+}) form and a feeding device was placed at the top of the resin bed. The temperature of the column, feed solution and eluant water was 65 °C. The flow rate in the column was adjusted to 210 l/h.

The pH of the feed solution was adjusted to pH 6.5 after which the solution was filtered via filter.

Chromatographic separation was carried out as follows:

Step 1.

The dry substance of the feed solution was adjusted to 30 g dry substance in 100 g of solution according to the refractive index (RI) of the solution.

Step 2.

110 l of the preheated feed solution was pumped to the top of the resin bed.

Step 3.

The feed solution was eluted downwards in the column by feeding preheated ion-exchanged water to the top of the column.

Step 4.

The density and conductivity of the outcoming solution were measured continuously. The outcoming solution was collected and divided into three fractions (when the feed profiles were not overlapping) in the following order: first residual fraction (containing components other than monosaccharides), rhamnose rich fraction (containing most of the rhamnose) and second residual fraction (containing other monosaccharides and other components).

The amount of dry substance as well as rhamnose content in the feed solution and in product fraction are presented in table 6. The concentration of rhamnose is expressed as percentage of the total dry substance in the particular fraction. The yield of rhamnose in product fraction is also presented

(the amount of the component in the particular fraction in relation to the total amount of that component in all outcoming fractions).

Table 6. : Compositions and yields

5

	<u>Feed solution</u> (nominal)	<u>Rhamnose fraction</u> (analysed from samples)
DS in fraction, kg	37	34.8
10 DS g/100 g solution	30	10.2
Rhamnose, %	47.9	55.4
Rhamnose, yield %		99.0

Rhamnose purity was increased by 16 %. Rhamnose yield was excellent being
15 99 %. The pH of the effluent was between 3.5 and 4. The results are shown graphically in FIG. 7.

Example 8

Crystallization of rhamnose

20 13100 g of a rhamnose syrup having DS of 14 % and a rhamnose content of 52.3 %, based on the refractometric dry solids content of pure rhamnose, was evaporated to RDS of 86.9 % and moved to a 2-liter reaction vessel at a temperature of 65 °C. Seeding (at 65 °C, a RDS of 86.9 %) was made to the boiling syrup with 0.03 % seeds on DS.

25 The mass was cooled down from a temperature of 65 °C to a temperature of 40 °C in 16 hours. After 16 hours from seeding, the centrifuging without wash gave a cake purity 98.5 % on RDS and a mother liquor purity 21.2 % on RDS, which corresponds to a 76 % rhamnose yield. The crystal size was 200... 350 µm. The moisture content of the dried crystals
30 was 10.0 % measured with a Karl Fischer titration method.

The results are shown in table 7.

Sample	RDS % by weight	Monosaccharides (PED LC) % on weight RDS						
		Rhamnose	Arabinose	Galactose	Glucose	Xylose	Mannose	Fructose
Feed	14.1	52.3	0.6	4.6	2.3	12.8	4.6	0.6
Mother liquor, no wash	54.3 *	21.2	0.7	7.8	4.0	21.3	7.8	1.0
Cake, no wash	90.0	98.5	-	0.1	0.0	0.3	0.1	-

* diluted sample

Example 9**Arabinose crystallization**

The arabinose containing feed liquid was added to a 400-litre boiling crystallizer. The evaporation was started at a temperature of 60 °C and at a pressure of 10 mbar. The boiling liquid was seeded with 0.03 % seeds on DS at DS of 67.9 % at a temperature of 60 °C and at a pressure of 130 mbar. After seeding the boiling crystallization was continued for 3 hours at a temperature of 60 °C and a new feed liquid was added continuously into the boiling crystallizer. A 400-litre batch of the mass obtained by boiling crystallization (DS of mass 68.9 %) was moved to a 400-litre cooling crystallizer.

The mass was cooled down from a temperature of 60 °C to a temperature of 30 °C in 20 hours. After cooling crystallization the mass was centrifuged. The crystals were dried and packed.